

DALLAS RANGEMASTER NOISE REDUCTION BUILD INSTRUCTIONS AND SIMULATION INFORMATION

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I recently did an in-depth analysis of the Dallas Rangemaster to determine why it was so susceptible to noise on the power line such as that from poor quality wall wart type power supplies. I published these results on the some guitar pedal builders groups on Facebook.

My conclusion was that a small change to the circuit consisting of two resistors and one capacitor would reduce the noise significantly while still preserving the unique audio characteristics if the circuit. The changes also allow it to run with a negative ground supply and make it suitable for use with daisy-chained pedal board supplies.

Under simulated conditions with 200mV peak to peak 100Hz ripple on the power line with the output measured at the half voltage setting of the output potentiometer this modification reduced the output noise from the circuit from 75mV to 400uV, that is an improvement by a factor of just under 200.

Since completing the work on the simulation and design change to reduce the Rangemaster's noise, I have designed a printed circuit board that allows the circuit to be built with the initial noise reduction modifications. The PCB also supports further standard modifications such as switchable input capacitors for changing the frequency response characteristics and changes to remove the DC content from the output potentiometer to minimise noise when adjusting the output level.

The next three pages have diagrams showing how to use the PCB to build out the circuit with various modifications plus also how to use the PCB to build the original Dallas Rangemaster for use with a negative ground (i.e. positive supply) to make it compatible with most modern guitar pedals so that it can be powered using a daisy chain power arrangement on a pedal board. All versions show the optional use of a 9v battery and have a true bypass switch included. Note that the original Dallas Rangemaster did not have a bypass switch or LED indicator, was permanently connected between the guitar and amplifier and only ran off battery power.

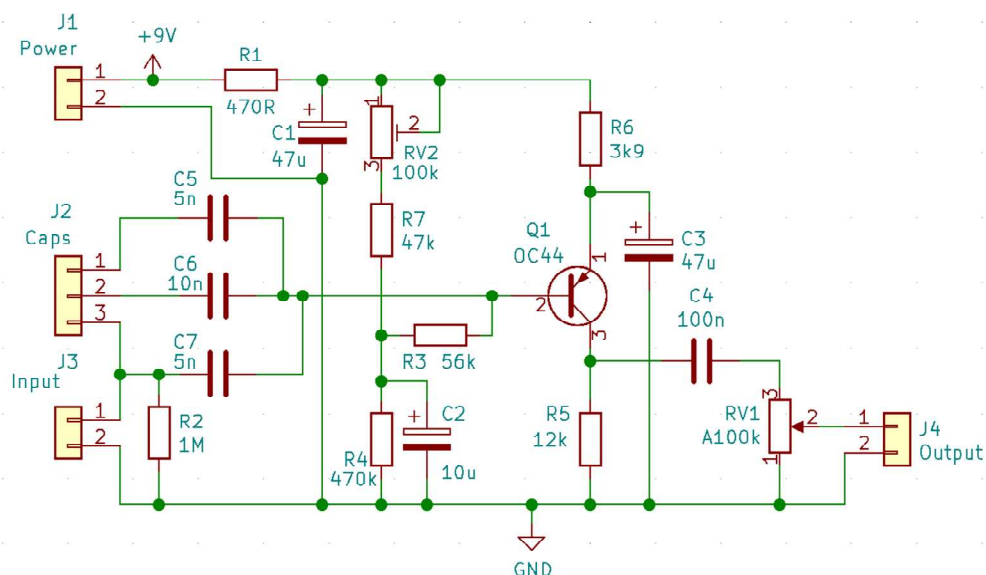
The last page of this document shows a fully annotated schematic of the setup used in simulation and describes the changes that will result in this improvement in performance. The circuit used for the LTSpice simulation clearly indicates what are part of the simulation test setup and the monitoring test points for data collection and what are the original and modified Rangemaster circuits.

It is important to note that these modifications to the Dallas Rangemaster circuit were designed so that they will not affect the original audio performance of the circuit and use the minimum number of additional components. They retain the original input impedance characteristics and they maintain the overall frequency response.

The changes to the design have been determined using an accurate simulation of the Rangemaster using an OC44 germanium transistor and a simulated Fender Stratocaster pickup and shunt capacitance on the input to simulate a typical length guitar cable.

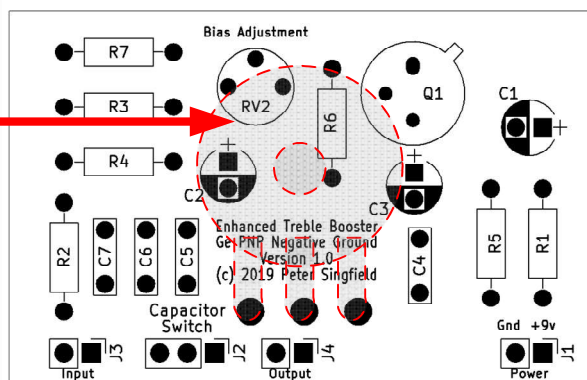
A simply change such as increasing the value of the 47uF capacitor on the power line of the original circuit has very little effect on the noise unless other changes are also made such as adding a series resistor in line with the power supply.

Schematic incorporating all the modifications

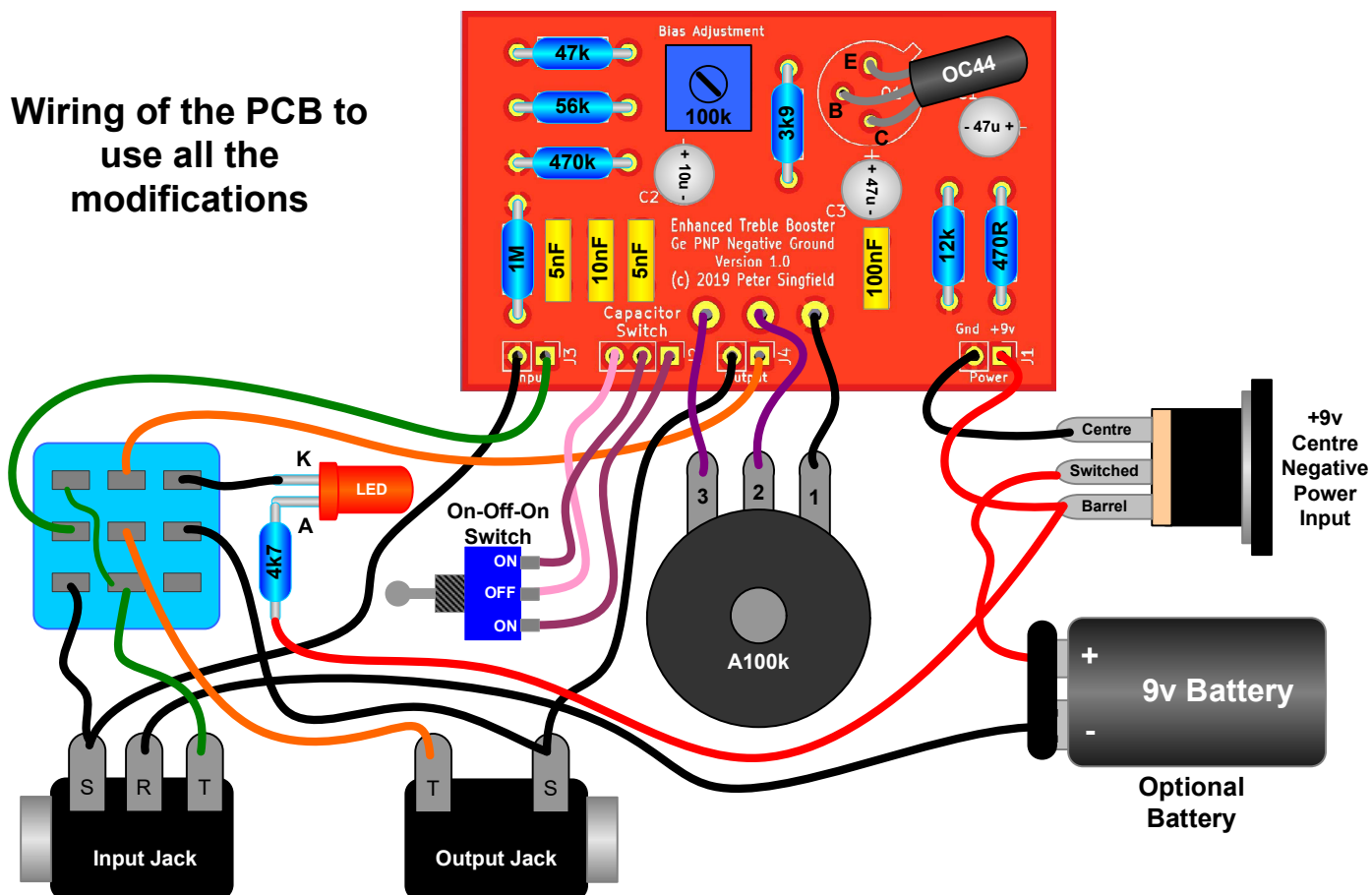


POT RV1 POSITIONED
UNDERNEATH PCB

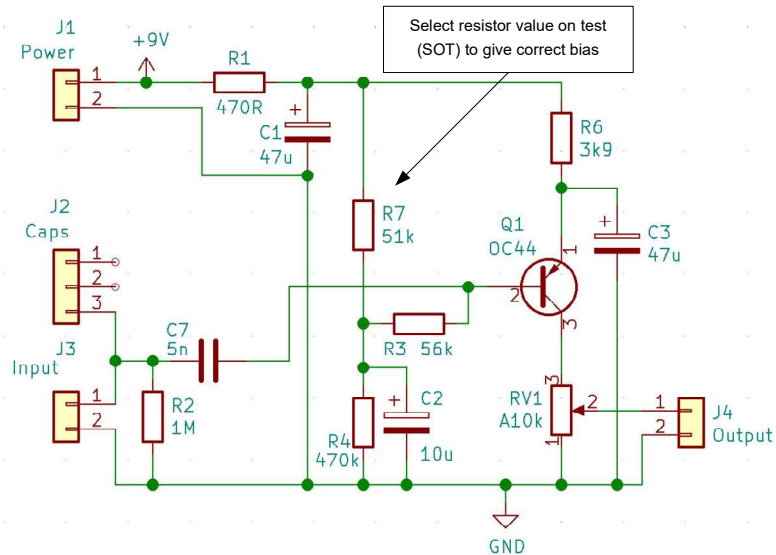
Component locations
on PCB



Wiring of the PCB to
use all the
modifications

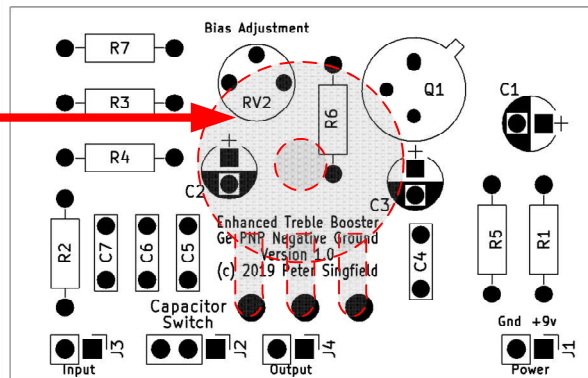


Schematic incorporating minimal modifications to reduce noise

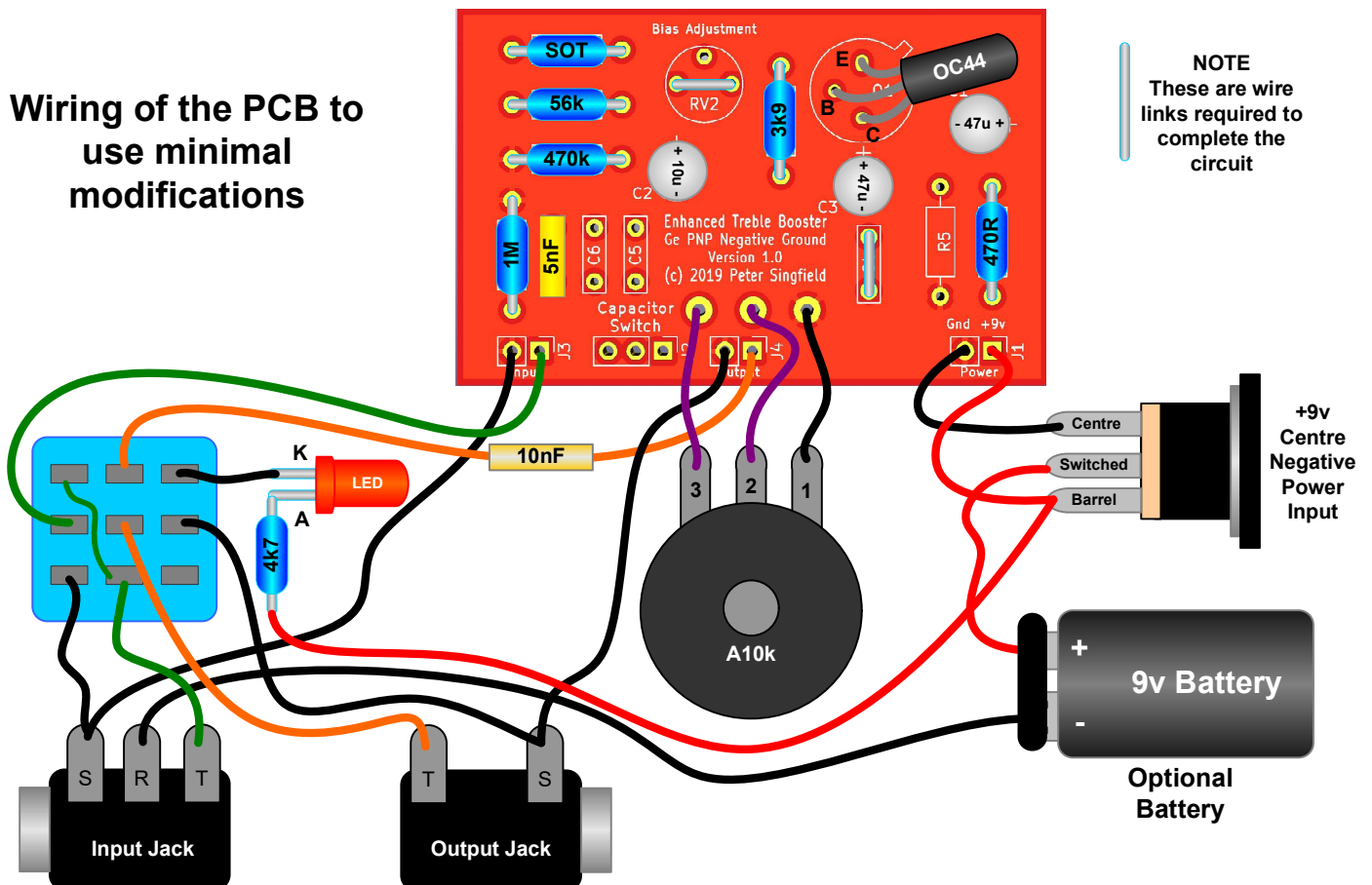


POT RV1 POSITIONED UNDERNEATH PCB

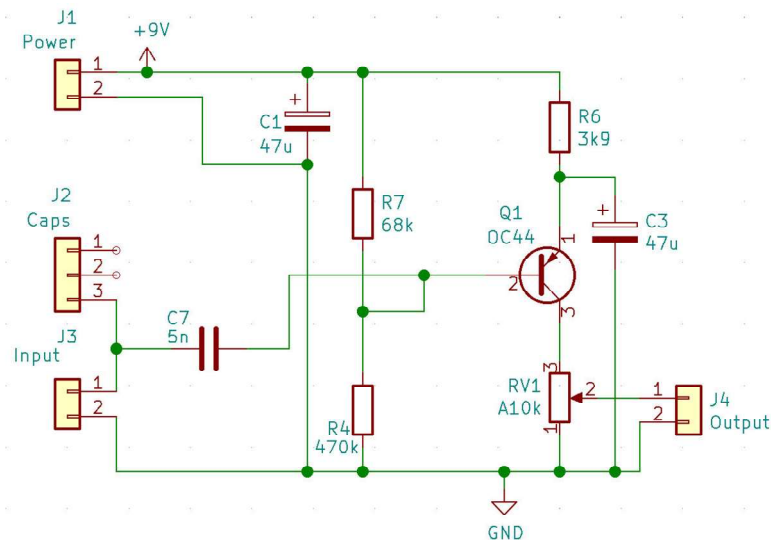
Component locations on PCB



Wiring of the PCB to use minimal modifications



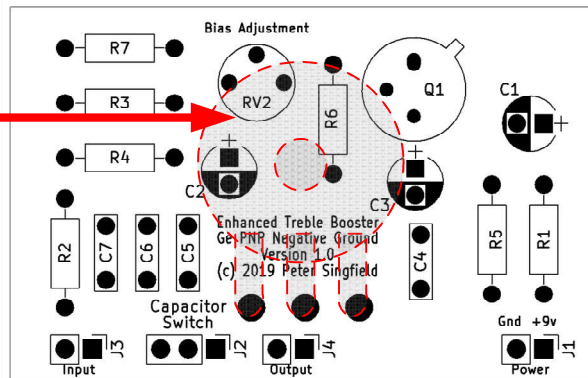
Schematic of original Rangemaster modified for negative ground



Requires external 10nF capacitor between PCB output and output jack

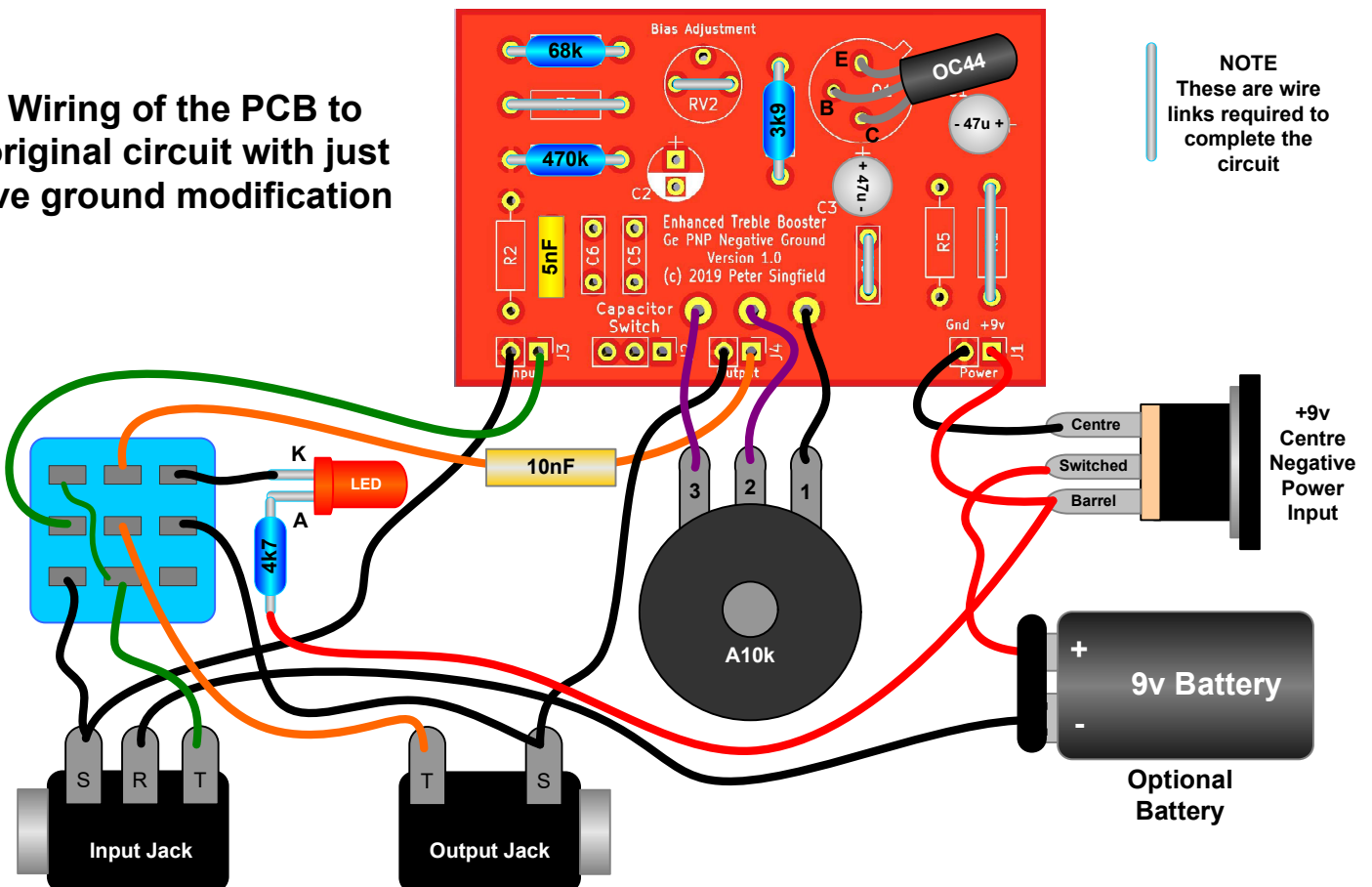
POT RV1 POSITIONED UNDERNEATH PCB

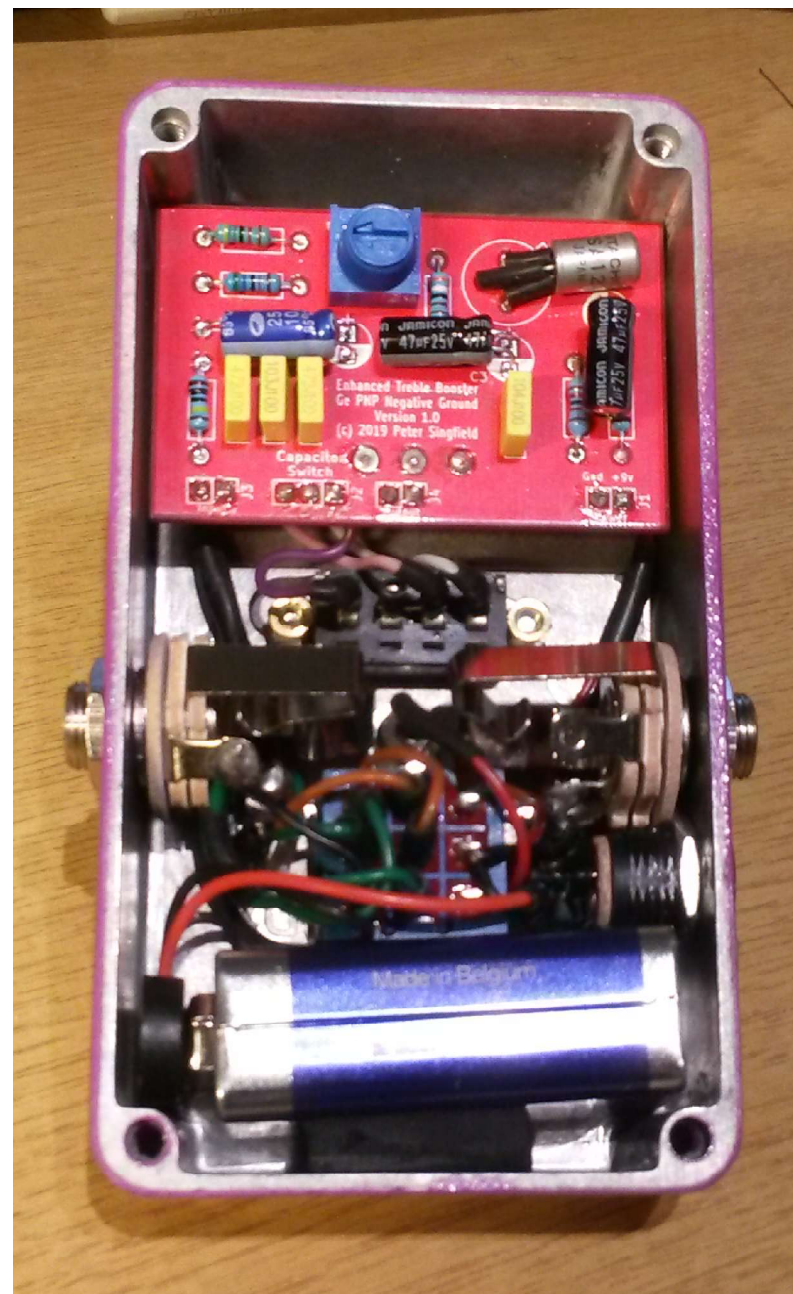
Component locations on PCB



Wiring of the PCB to original circuit with just -ve ground modification

NOTE
These are wire links required to complete the circuit





LTSpice Simulation Setup

NOTE

These components are here to allow the ripple voltage to be monitored in LTSpice. The use of 100k resistors mean they have negligible effect on the performance of power line filtering

This generates 200mV p-p ripple at 100Hz

These are the modifications required

470 ohm resistor added to form 7Hz RC low pass filter on power line

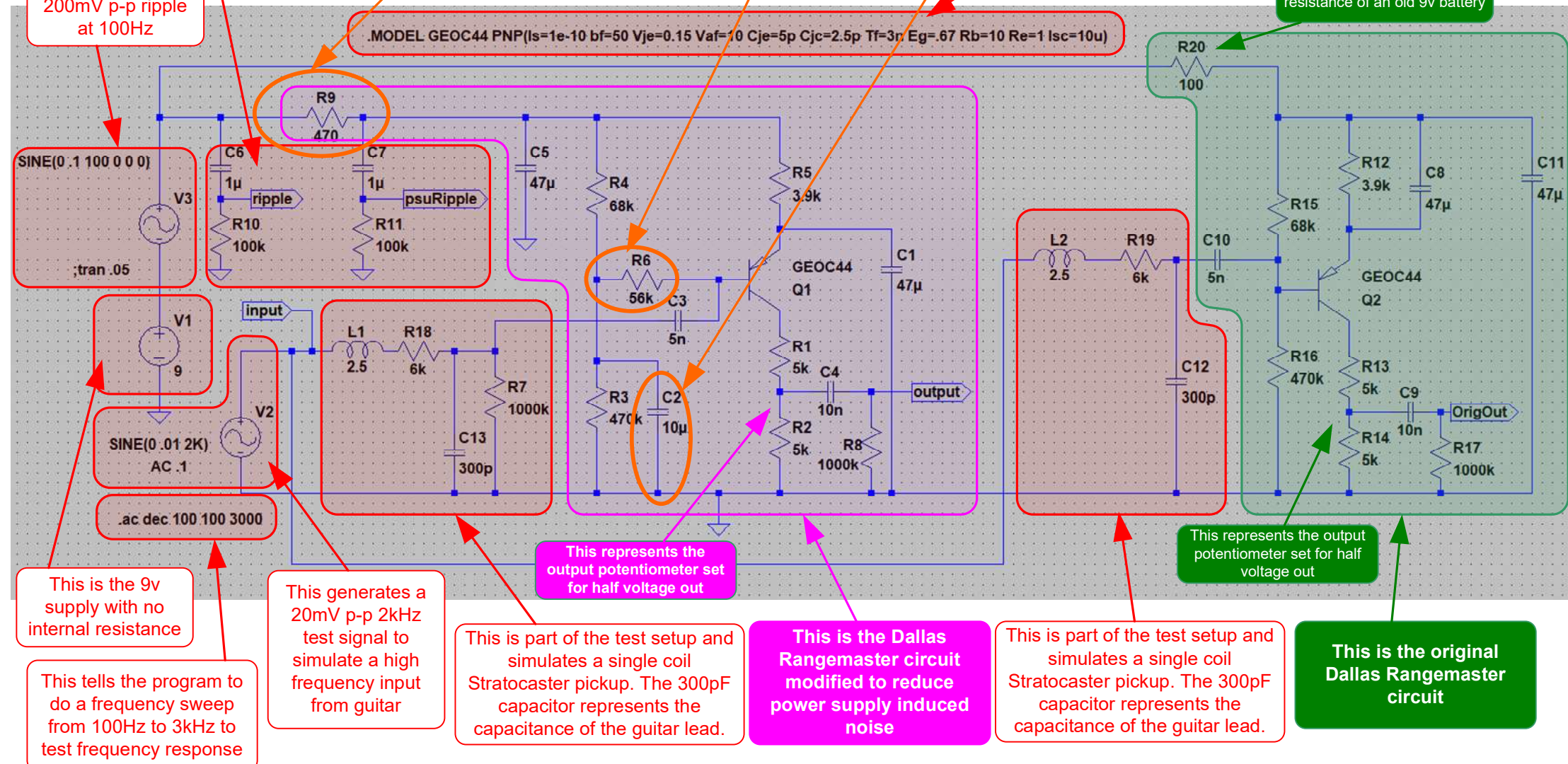
Resistor added to isolate transistor input from bias network whilst maintaining original input impedance characteristics

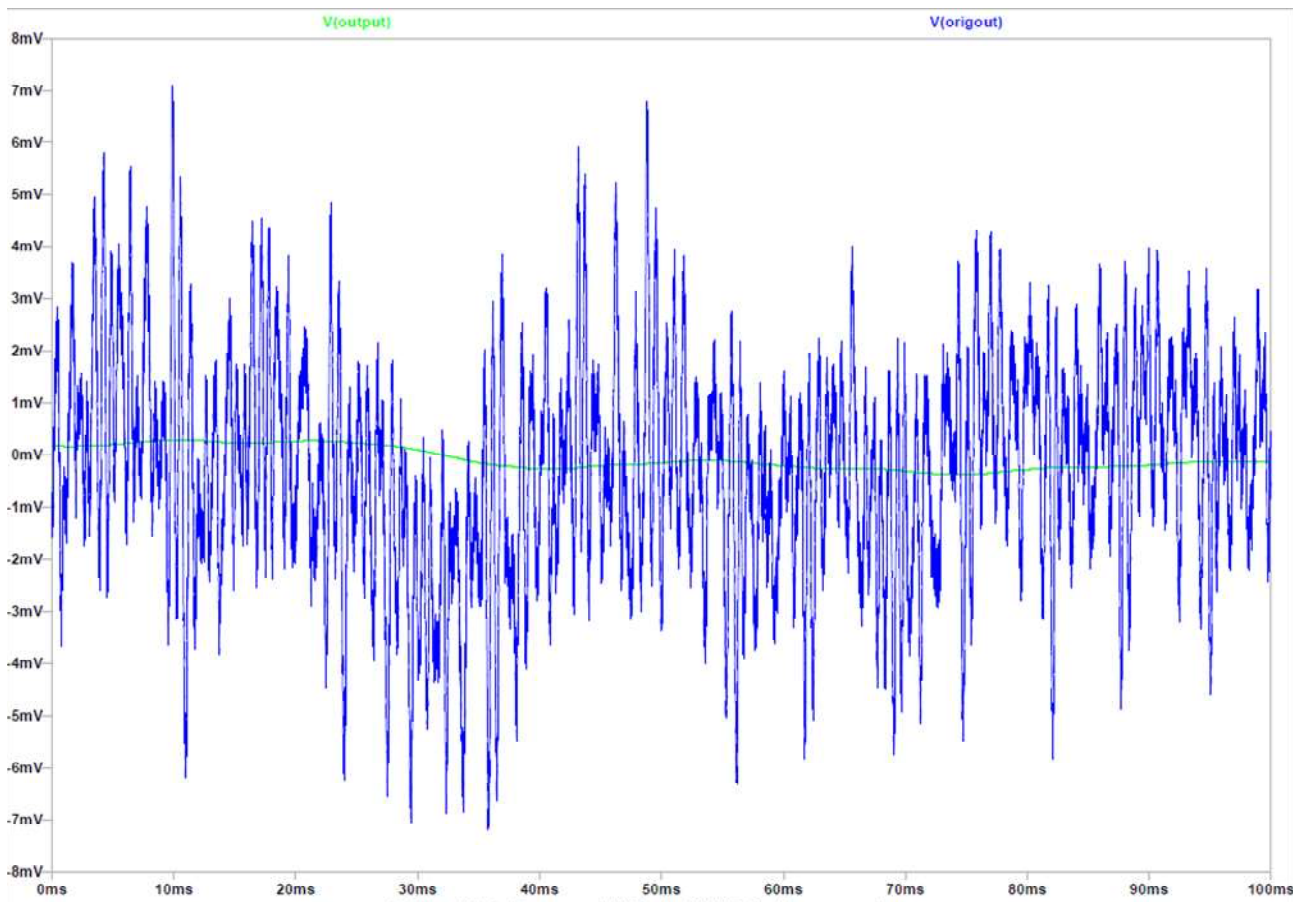
Capacitor added decouple bias network and filter noise from transistor bias voltage effectively forming a virtual ground

These parameters used to model OC44 Germanium PNP transistor

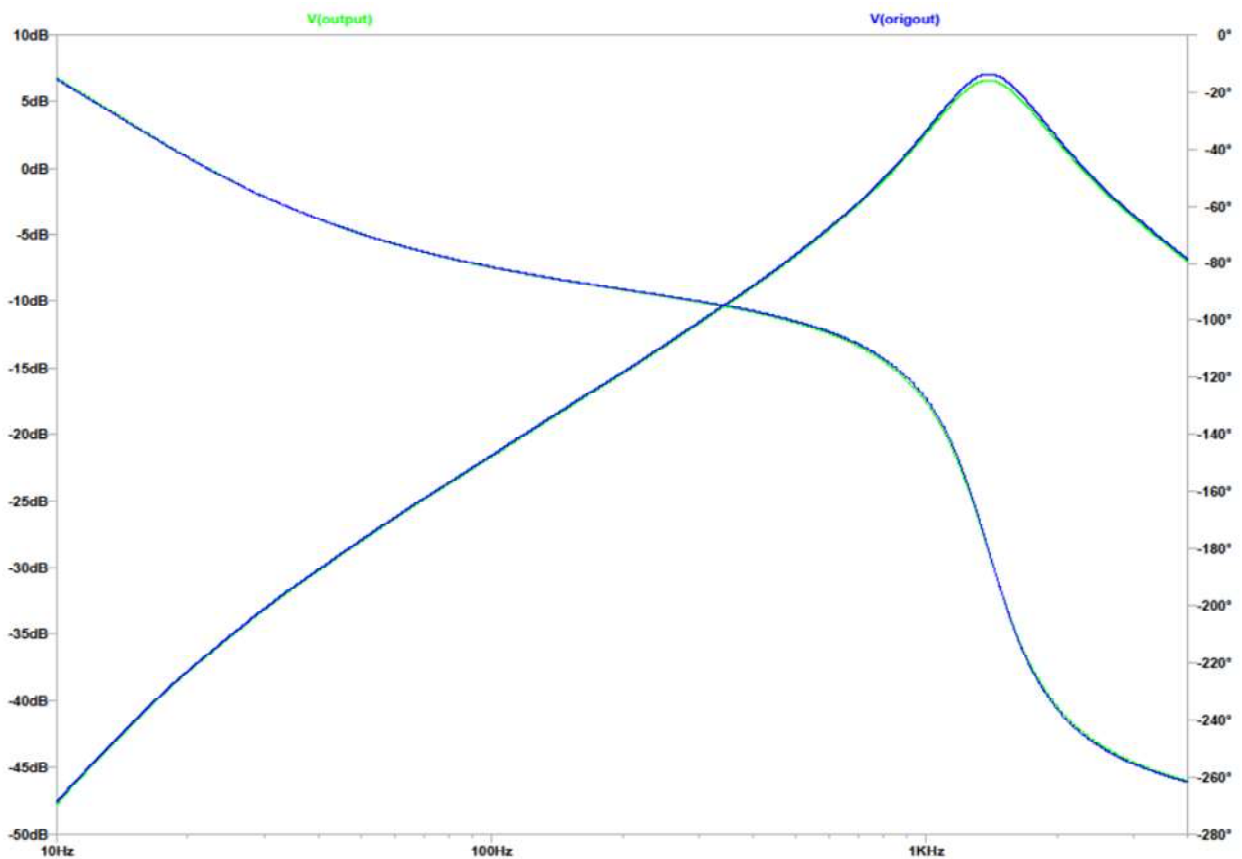
This represents the internal resistance of an old 9v battery

.MODEL GEOC44 PNP(Is=1e-10 bf=50 Vje=0.15 Vaf=10 Cje=5p Cjc=2.5p Tf=3n Eg=.67 Rb=10 Re=1 Isc=10u)

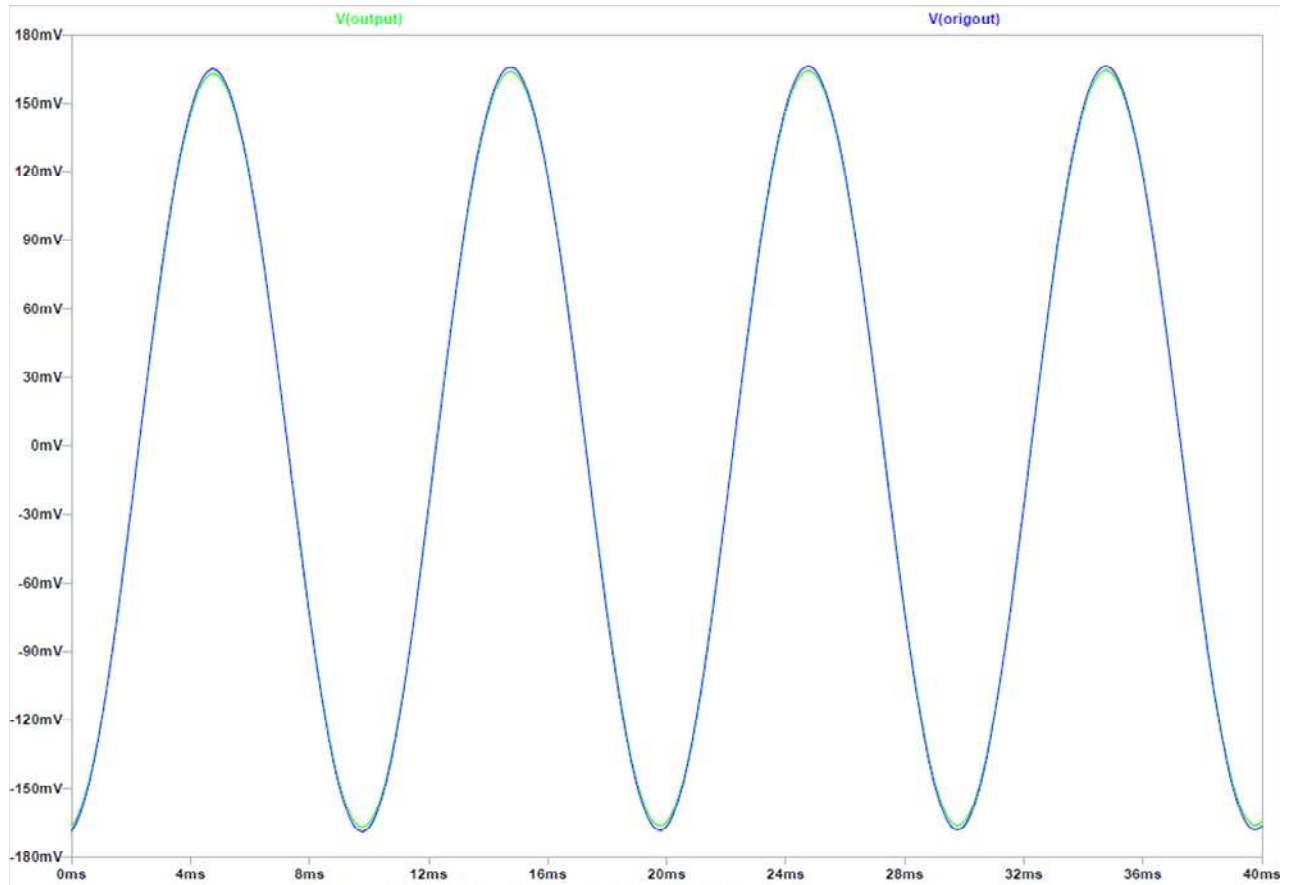




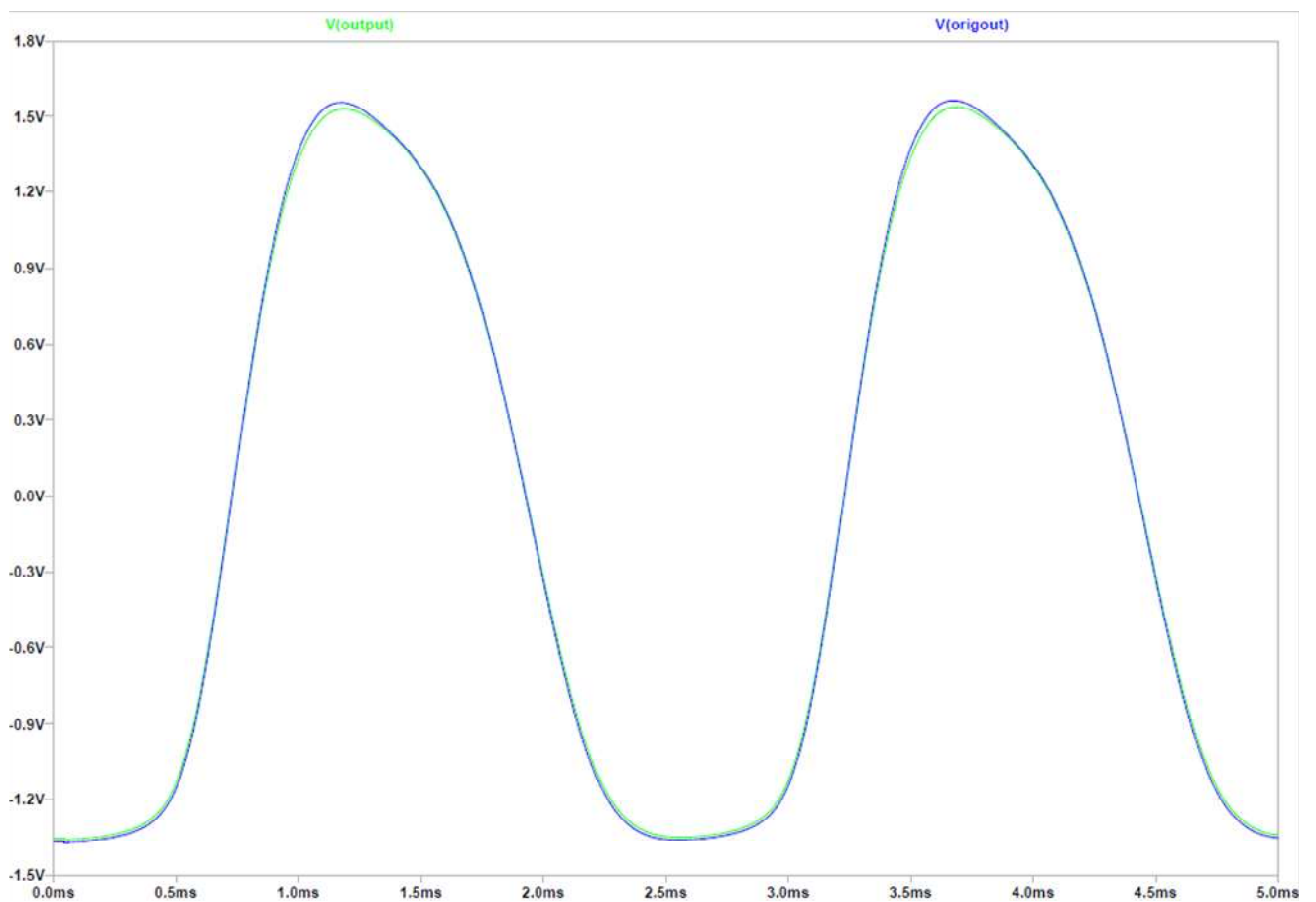
Output of original (blue) and modified (green) circuits with 0.5v p-p noise on power supply



Frequency response of original (blue) and modified (green) circuits



100Hz sine wave output of original (blue) and modified (green) circuits



400Hz overdriven output of original (blue) and modified (green) circuits